

Combined Speed and Current Model Predictive Control with Inherent Field-Weakening Features for PMSM Drives

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Key idea of MPC

Model Predictive controllers rely on the fact that the available model of the system is rich and accurate enough to

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- 1 predict the future behavior of the outputs

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Model Predictive controllers rely on the fact that the available model of the system is rich and accurate enough to

- 1 predict the future behavior of the outputs
- 2 choose the inputs so that the future behavior
 - minimizes a given cost function
 - satisfies given constraints

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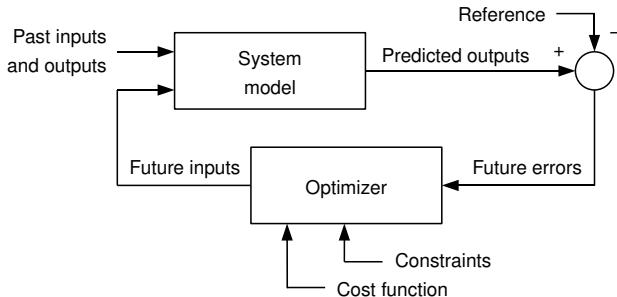
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Receding horizon strategy

One of the key strategies of MPC is the receding horizon idea.

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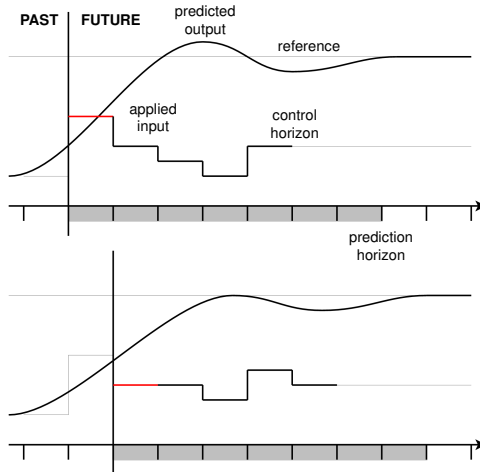
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One of the mathematical framework that can be used for MPC is **state space (linear) modeling** with linear constraints.

$$\mathbf{x}(k+1) = \mathbf{Ax}(k) + \mathbf{Bu}(k)$$

$$\mathbf{y}(k) = \mathbf{Cx}(k) + \mathbf{Du}(k)$$

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$$\mathbf{x}(k+1) = \mathbf{A}\mathbf{x}(k) + \mathbf{B}\mathbf{u}(k)$$

$$\mathbf{y}(k) = \mathbf{C}\mathbf{x}(k) + \mathbf{D}\mathbf{u}(k)$$

$$\mathbf{x} \in \mathbf{X} \subset \mathbb{R}^n, \mathbf{y} \in \mathbf{Y} \subset \mathbb{R}^p, \mathbf{u} \in \mathbf{U} \subset \mathbb{R}^m$$

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$$\mathbf{x} \in \mathbf{X} \subset \mathbb{R}^n, \mathbf{y} \in \mathbf{Y} \subset \mathbb{R}^p, \mathbf{u} \in \mathbf{U} \subset \mathbb{R}^m$$

The **cost function** that has to be minimized, generally takes the quadratic form

$$J_{N_p} = \sum_{j=k}^{k+N_p-1} \left[\mathbf{x}(j)^T \mathbf{Q}\mathbf{x}(j) + \mathbf{u}(j)^T \mathbf{R}\mathbf{u}(j) \right]$$

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This setup simplifies the resulting control law.

Fields of application

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Model Predictive Control is particularly effective for plants that:

- can be modelled with a simple, known, system (possibly linear + time delays)

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Model Predictive Control is particularly effective for plants that:

- can be modelled with a simple, known, system (possibly linear + time delays)
- constraints play a critical role in the system dynamics

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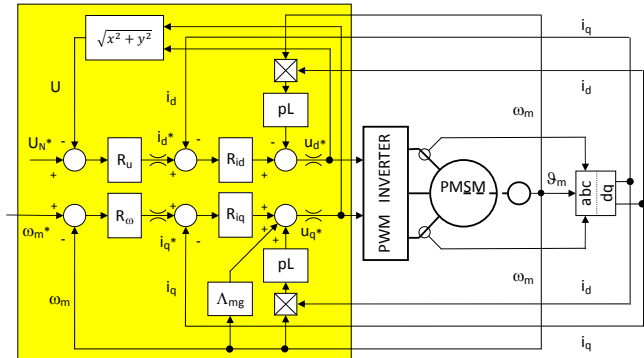
Model Predictive Control is particularly effective for plants that:

- can be modelled with a simple, known, system (possibly linear + time delays)
- constraints play a critical role in the system dynamics
- have multiple inputs / outputs / states
- have long time constants

Electrical drives fit in this category!

Once faster hardware and algorithm are available, MPC can be considered when designing an electrical motor drive, for example for a PMSM drive.

Controller structure



PID cascade controller

Classical solution: an inner loop for the current control and an outer loop for speed control. Bounds are enforced in every controller and flux weakening requires an external algorithm.

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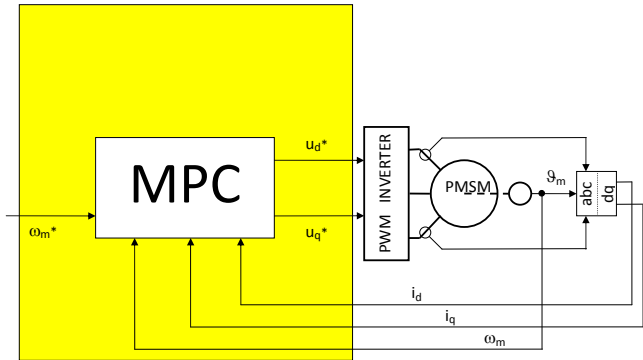
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Controller structure



One MPC single controller

One only MPC controller is driven by the speed reference and commands the voltages that feed the motor. Bounds are enforced inside the controller.

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Permanent Magnet Synchronous Motor equations

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The electrical and mechanical dynamics of a PMSM motor is described by the following equations in the ($d - q$) synchronous reference frame

$$\frac{di_d}{dt} = \frac{1}{L} (u_d - Ri_d + \omega_{me}Li_q)$$
$$\frac{di_q}{dt} = \frac{1}{L} (u_q - Ri_q - \omega_{me}Li_d - \omega_{me}\Lambda_{mg})$$

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$$\begin{aligned}\frac{di_d}{dt} &= \frac{1}{L} (u_d - Ri_d + \omega_{me}Li_q) \\ \frac{di_q}{dt} &= \frac{1}{L} (u_q - Ri_q - \omega_{me}Li_d - \omega_{me}\Lambda_{mg}) \\ \frac{d\omega_{me}}{dt} &= \frac{p}{J} \left(k_t i_q - \frac{B}{p} \omega_{me} - \tau_L \right)\end{aligned}$$

Permanent Magnet Synchronous Motor equations

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which are continuous-time, non linear equations, even if iron saturation is assumed negligible (constant parameters), because of the **motional coupling terms**.

Linearized discrete-time model

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The first step in MPC design consists in obtaining a linear, discrete-time model for the system. This mainly means getting rid of the motional coupling terms $\omega_{me}Li_d$ and $\omega_{me}Li_q$.

$$\mathbf{x} = \left[i_d \quad i_q \quad \widehat{\omega_{me}Li_q} \quad \omega_{me} \right]^T$$

$$\frac{d\mathbf{x}}{dt} = \begin{bmatrix} -\frac{R}{L} & 0 & 1 & 0 \\ -\omega_B & -\frac{R}{L} & 0 & -\frac{\Lambda_{mg}}{L} \\ 0 & 0 & 0 & 0 \\ 0 & \frac{pk_t}{J} & 0 & -\frac{B}{J} \end{bmatrix} \mathbf{x} + \begin{bmatrix} \frac{1}{L} & 0 \\ 0 & \frac{1}{L} \\ 0 & 0 \\ 0 & 0 \end{bmatrix} \mathbf{u}$$

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One can consider these terms as a measured disturbance. It has been done for $\omega_{me}Li_q$.

Linearized discrete-time model

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One can consider these terms as a measured disturbance. It has been done for $\omega_{me}Li_q$. **Something different has been done for the $\omega_{me}Li_d$ term, linearizing it around the base speed ω_B .**

Linearized discrete-time model

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One can consider these terms as a measured disturbance. It has been done for $\omega_{me}Li_q$. Something different has been done for the $\omega_{me}Li_d$ term, linearizing it around the base speed ω_B . Linearization then follows standard Euler techniques.

State augmentation for tracking

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There are a couple of modification that are needed to achieve reference tracking.

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There are a couple of modification that are needed to achieve reference tracking.

- the reference ω_{me}^{ref} has to appear as a state variable (we'll assume it is constant in the prediction interval)

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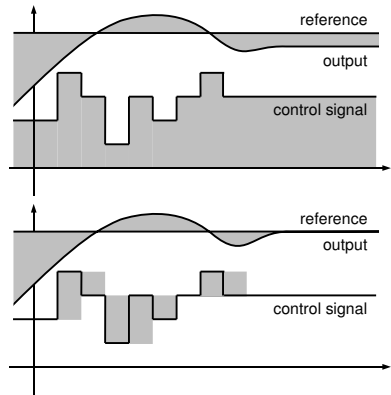
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There are a couple of modification that are needed to achieve reference tracking.

- the reference ω_{me}^{ref} has to appear as a state variable (we'll assume it is constant in the prediction interval)
- the input variation Δu is weighted instead of u (to achieve offset-free tracking)



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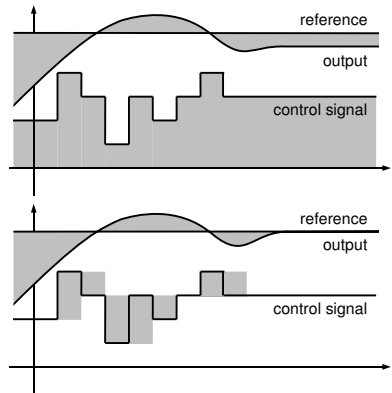
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There are a couple of modification that are needed to achieve reference tracking.

- the reference ω_{me}^{ref} has to appear as a state variable (we'll assume it is constant in the prediction interval)
- the input variation $\Delta \mathbf{u}$ is weighted instead of \mathbf{u} (to achieve offset-free tracking)



After this augmentation, the system state has dimension 7.

Input and state constraints

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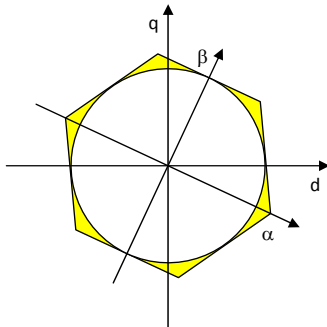
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The second step consists in defining the input and state constraints of the system.

Due to inverter limitation, the voltage vector has to stay inside an hexagon which is fixed in the $\alpha - \beta$ reference frame. In the $d - q$ frame this can be approximated by a circular region.

Input and state constraints

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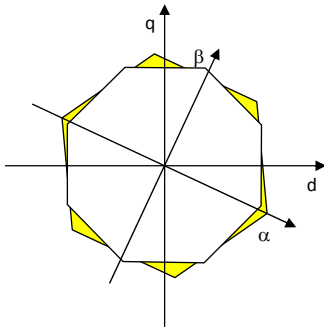
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Due to inverter limitation, the voltage vector has to stay inside an hexagon which is fixed in the $\alpha - \beta$ reference frame. In the $d - q$ frame this can be approximated by a circular region.

To have linear constraints in the $d - q$ frame, an octagonal region is adopted.

Cost function

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Once the model of the system is fully defined, the cost function has to be tuned.

$$J_{N_p} = \sum_{j=k}^{k+N_p-1} \left[\mathbf{x}(j)^T \mathbf{Q} \mathbf{x}(j) + \mathbf{u}(j)^T \mathbf{R} \mathbf{u}(j) \right]$$

Cost function

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There are two main degrees of freedom

- the prediction horizon length N_p ($N_p = 5$ resulted to be a good tradeoff between enclosing most of the system dynamics and keeping the computational effort low)

Cost function

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There are two main degrees of freedom

- the prediction horizon length N_p ($N_p = 5$ resulted to be a good tradeoff between enclosing most of the system dynamics and keeping the computational effort low)
- the weigh matrices \mathbf{Q} and \mathbf{R}

Cost function

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The matrices **Q** and **R** contain weighting coefficients for the state variables and the input signals.

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The matrices **Q** and **R** contain weighting coefficients for the state variables and the input signals.

- γ_{i_d}
penalizes the direct current i_d , so that it is kept to zero unless it is really needed (i.e. for flux weakening)

Cost function

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The matrices **Q** and **R** contain weighting coefficients for the state variables and the input signals.

- γ_{i_d}
- γ_{i_q}
slightly penalizes the quadrature current i_q (mainly for stability purposes)

Cost function

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- γ_{i_d}

- γ_{i_q}

- $\gamma_{\omega_{me}}$

weighs the speed error with respect to the gived speed reference

Cost function

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- γ_{i_d}

- γ_{i_q}

- $\gamma_{\omega_{me}}$

- $\gamma_{\Delta u_d}$ and $\gamma_{\Delta u_q}$

weights the input signal variations (it has to be non-zero to have unique solution of the optimization problem)

Cost function

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- γ_{i_d}
- γ_{i_q}
- $\gamma_{\omega_{me}}$
- $\gamma_{\Delta u_d}$ and $\gamma_{\Delta u_q}$

These parameters are mainly tuned in a trial-and-error process based on simulations.

Affine state feedback control law

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Finding the optimal inputs is Quadratic Programming

Having a linear system with linear constraints and a quadratic cost function, allows to solve the optimization problem with the standard tools of QP.

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Finding the optimal inputs is Quadratic Programming

Having a linear system with linear constraints and a quadratic cost function, allows to solve the optimization problem with the standard tools of QP.

Moreover, the resulting control that is commanded (the first sample of the optimal input sequence) results to be an **affine feedback of the state**

$$\Delta \mathbf{u}_i(k) = \mathbf{F}_i \mathbf{x}(k) + \mathbf{G}_i$$

Affine state feedback control law

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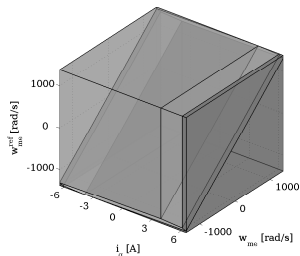
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Finding the optimal inputs is Quadratic Programming

Having a linear system with linear constraints and a quadratic cost function, allows to solve the optimization problem with the standard tools of QP.

Moreover, the resulting control that is commanded (the first sample of the optimal input sequence) results to be an affine feedback of the state defined in different **regions of the state space**.

$$\Delta \mathbf{u}_i(k) = \mathbf{F}_i \mathbf{x}(k) + \mathbf{G}_i$$



Algorithm

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The control algorithm then consists in

- 1 finding the active region
- 2 applying the corresponding feedback law

$$\Delta \mathbf{u}_i(k) = \mathbf{F}_i \mathbf{x}(k) + \mathbf{G}_i$$

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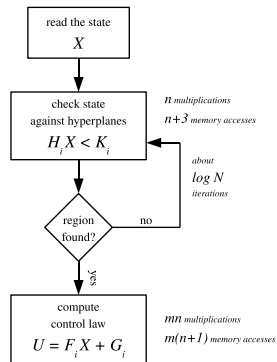
The control algorithm then consists in

- 1 finding the active region
- 2 applying the corresponding feedback law

$$\Delta \mathbf{u}_i(k) = \mathbf{F}_i \mathbf{x}(k) + \mathbf{G}_i$$

It is not necessary to inspect all the regions! A dichotomic search can be done comparing the current state against a series of hyperplanes.

A binary search tree is built off-line. The online part of the algorithm is minimal!



Test bench

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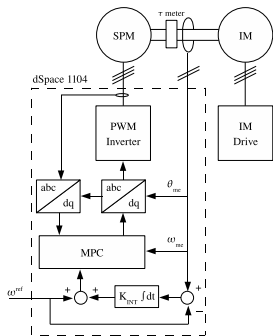
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The MPC controller we just designed has been implemented on a dSpace 1104 fast prototyping board.

The *Multi Parametric Toolbox (MPT)* for *Matlab* provides both a solver for the optimization problem and some routines to generate the region partition and the binary search tree for simulation and actual implementation.

1st test

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Speed reference step 1200 to 1800 rpm – no FW is needed.

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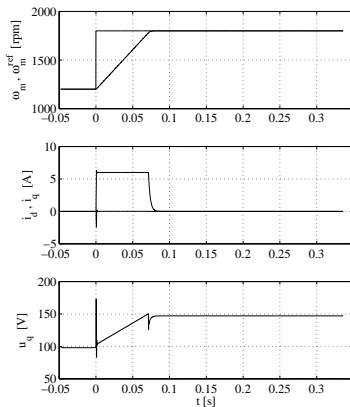
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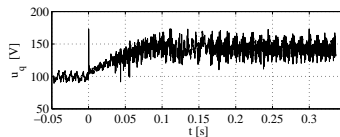
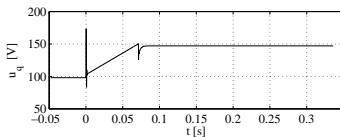
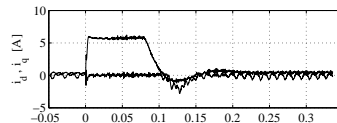
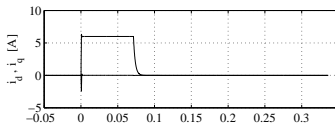
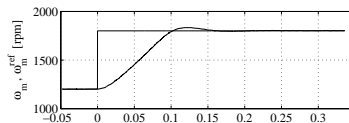
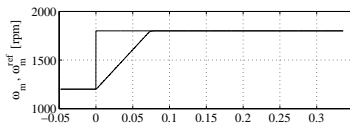
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Speed reference step 1800 to 2400 rpm – FW is needed.

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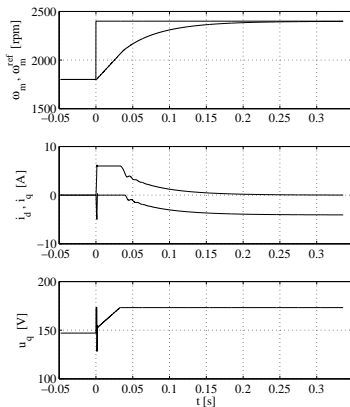
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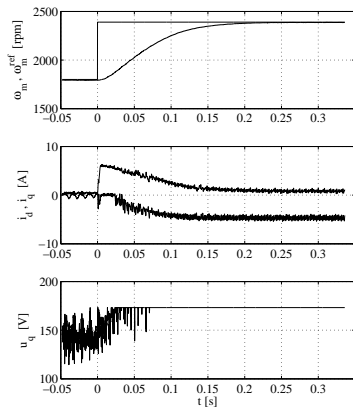
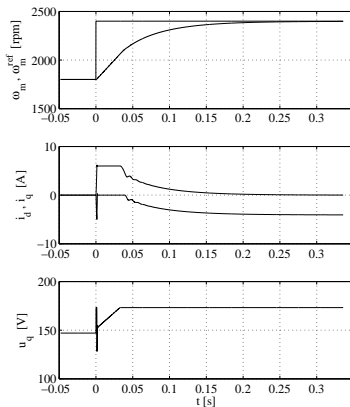
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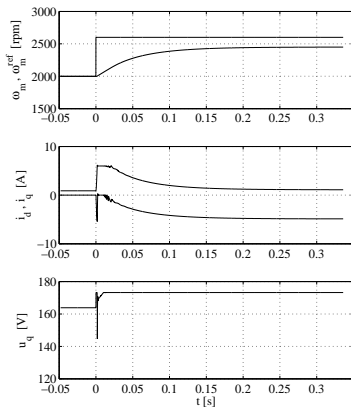
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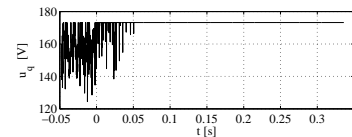
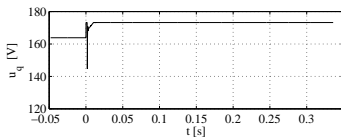
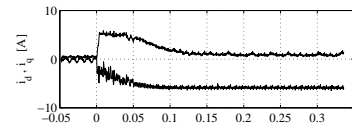
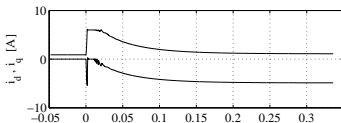
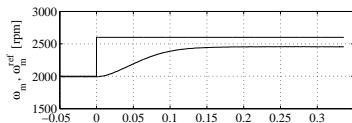
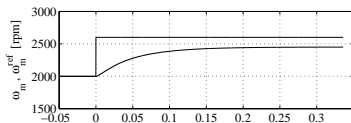
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The proposed MPC controller for both speed and current of a PMSM drive, is able to command the motor both below and above base speed, by an effective and inherent flux weakening.

Details of the design, of the control algorithm generation, and of the actual implementation have been provided in the paper.

Simulation and experimental results prove the promising performance of the proposed controller.

Pros and Cons

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Pros:

- one single controller effectively drives the motor in all its operating regions
- bounds are automatically enforced, with no need of saturations and anti-windup strategies
- more complex cost functions may be adopted
- reference and load dynamics can be added in the model

Pros and Cons

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Pros:

- one single controller effectively drives the motor in all its operating regions
- bounds are automatically enforced, with no need of saturations and anti-windup strategies
- more complex cost functions may be adopted
- reference and load dynamics can be added in the model

Cons:

- the computational effort is higher than most of the conventional controllers
- drive and controller parameter changes require off-line algorithm tuning
- model mismatch has to be taken into account

Possible future works

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This is the first complete application of MPC to current/speed control of a PMSM drive with flux weakening

Some interesting issues arose and are worth investigation.

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This is the first complete application of MPC to current/speed control of a PMSM drive with flux weakening

Some interesting issues arose and are worth investigation.

- testing on different drives, SPM motors with wider flux weakening region, IPM motors

Possible future works

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Some interesting issues arose and are worth investigation.

- testing on different drives, SPM motors with wider flux weakening region, IPM motors
- direct implementation with FPGA

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Some interesting issues arose and are worth investigation.

- testing on different drives, SPM motors with wider flux weakening region, IPM motors
- direct implementation with FPGA
- stability and robustness analysis with respect to parameters mismatch

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Thank you!