

A Control Matching Model Predictive Control Approach to String Stable Vehicle Platooning

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Lecture content

- 1 Modeling and notation
- 2 Control objective, constraints and requirements
- 3 MPC problem formulation
- 4 Control matching
- 5 Experimental results

Note: The following notes have been extracted from “A Control Matching Model Predictive Control Approach to String Stable Vehicle Platooning”, Roozbeh Kianfar, Paolo Falcone, Jonas Fredriksson. *Submitted to Control Engineering Practice.*

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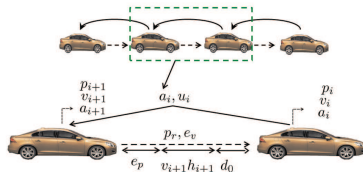
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Modeling and notation

Consider the platoon in the figure. Model the i -th vehicle as ($i = 1, \dots, N$):

$$\begin{aligned}\dot{e}_{p,i} &= e_{v,i} - a_i h_i, \\ \dot{e}_{v,i} &= a_{i-1} - a_i, \\ a_i &= \frac{K_i}{\tau_i s + 1} e^{-\theta_i s} a_i^{\text{des}},\end{aligned}$$



The resulting model is $\dot{x}(t) = Ax(t) + B_u u(t - \theta) + B_\omega \omega(t)$, with

$$\begin{aligned}x &= \begin{bmatrix} e_{p,i} & e_{v,i} & a_i & v_i \end{bmatrix}^T, \\ u_i &= a_i^{\text{des}}, \\ \omega &= a_{i-1},\end{aligned}$$

$$\begin{aligned}A &= \begin{bmatrix} 0 & 1 & -h_i & 0 \\ 0 & 0 & -1 & 0 \\ 0 & 0 & -1/\tau_i & 0 \\ 0 & 0 & 1 & 0 \end{bmatrix}, \\ B_u &= \begin{bmatrix} 0 \\ 0 \\ \frac{K_i}{\tau_i} \\ 0 \end{bmatrix}, B_\omega = \begin{bmatrix} 0 \\ 1 \\ 0 \\ 0 \end{bmatrix},\end{aligned}$$

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Control objective, constraints and requirements

Problem statement. Minimizing the position and velocity errors while satisfying a performance (e.g., string stability and smooth driving) and safety requirements (e.g., rear-end collision avoidance).

- 1 **Safety.** A safe *minimum* distance must be maintained from the preceding vehicle in order to prevent rear-end collisions

$$e_{p,\min} \leq e_{p,i}(t) \leq e_{p,\max}, \quad \forall t \geq 0.$$

- 2 **Performance (comfort).**

- ▶ Bounds on *relative velocities*

$$e_{v,\min} \leq e_{v,i}(t) \leq e_{v,\max}, \quad \forall t \geq 0,$$

- ▶ **Max velocity** $0 \leq v_i(t) \leq v_{\max}, \quad \forall t \geq 0,$
- ▶ **Acceleration**

$$a_{\min} \leq a_i(t) \leq a_{\max}, \quad \forall t \geq 0,$$

- 3 **Physical limitation.** Max acceleration demands imposed by the powertrain

$$u_{\min} \leq u_i(t) \leq u_{\max}, \quad \forall t \geq 0.$$

Control objective, constraints and requirements

Constraints 1-3 can be compactly written as

$$\begin{bmatrix} H_x & H_u \end{bmatrix} \begin{bmatrix} x \\ u \end{bmatrix} \leq h_x.$$

Definition

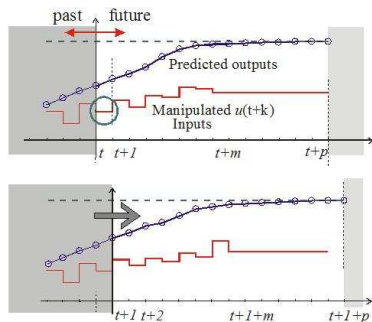
A vehicle platoon is predecessor-follower string stable w.r.t. an acceleration disturbance if

$$\|\Gamma_i(s)\|_\infty = \sup_{a_{i-1} \neq 0} \frac{\|a_i(t)\|_{\mathcal{L}_2}}{\|a_{i-1}(t)\|_{\mathcal{L}_2}}.$$

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MPC problem formulation. Background



- 1 Every sampling time solve a *CFTOC, based on the current state*
- 2 Apply the optimal input *only in $[t, t + 1]$*
- 3 At $t + 1$ solve a CFTOC over a *shifted horizon* based on new state measurements

- 4 The resulting controller is referred to as *Receding Horizon Controller (RHC)*.
- 5 If the finite time optimal control law is computed by solving an optimization problem on-line, the RHC is usually referred to as *Model Predictive Control (MPC)*.

MPC problem formulation

$$J(x(t), \omega(t)) = \min_{U_t} \quad \|Px(N|t)\|_2 \\ + \sum_{k=0}^{N-1} \|Qx(t+k|t)\|_2 + \|Ru(t+k|t)\|_2$$

subj. to

$$x_{t+k+1,t} = F_i x_{t+k,t} + G_{1,i} u_{t+k,t} + G_{2,i} \omega_{t+k,t},$$

$$\begin{bmatrix} H_x & H_u \end{bmatrix} \begin{bmatrix} x_{t+k,t} \\ u_{t+k,t} \end{bmatrix} \leq h_x,$$

$$x_{t+N,t} \in \mathcal{X}_f = \mathbb{R}^n$$

$$\omega_{t+k|t} = \omega_{t|t}$$

$$k = [0, \dots, N-1],$$

$$\omega_{t,t} = \omega(t),$$

$$x_{t,t} = x(t),$$

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Control matching

Basic idea

- 1 Design a string stable linear controller
- 2 “Tune” the weighting matrices Q , P , R in order to retrieve the behavior of the string stable linear controller.

Step 1. Consider the feedback/feedforward control policy,

$$u_{ss,i} = K^{ss} \begin{bmatrix} x \\ \omega \end{bmatrix} = [K_{\text{FB}}^{ss} \ K_{\text{FF}}^{ss}] \begin{bmatrix} x \\ \omega \end{bmatrix},$$

where K_{FB}^{ss} and K_{FF}^{ss} are static state feedback and feedforward gains.

The closed-loop dynamics are $\dot{x}(t) = A^{\text{cl}}x(t) + E_{\omega}^{\text{cl}}\omega(t)$, where $A^{\text{cl}} = A + B_u K_{\text{FB}}^{ss}$ and $E_{\omega}^{\text{cl}} = B_u K_{\text{FF}}^{ss} + B_{\omega}$. Consider the following output signals,

$$\begin{bmatrix} a_i \\ e_{p,i} \\ u_{ss,i} \end{bmatrix} = \begin{bmatrix} C_{\Gamma} & D_{\Gamma} \\ C_H & D_H \end{bmatrix} \begin{bmatrix} x \\ \omega \end{bmatrix}.$$

Control matching

Define the transfer functions

- ❶ $\Gamma = C_\Gamma (sI - A^{\text{cl}})^{-1} E_\omega^{\text{cl}} + D_\Gamma$, the transfer function from ω to a_i ,
- ❷ $H = C_H (sI - A^{\text{cl}})^{-1} E_\omega^{\text{cl}} + D_H$, the transfer function from ω to $[e_{p,i} \ u_{ss,i}]^T$.

Calculate K^{ss} as,

$$\begin{aligned} K^{ss} = \underset{K^{ss}}{\operatorname{argmin}} \quad & \alpha \|\Gamma\|_\infty + \beta \|H\|_2, \\ \text{subj.to} \quad & \|\Gamma\|_\infty \leq 1, \end{aligned}$$

Step 2. Rewrite the MPC problem as

$$\begin{aligned} J(x(k), \omega(k), U(k)) = \min_{U(k)} & U(k)^T H U(k) \\ & + 2x(k)^T F U(k) + x(k)^T Y x(k) \\ \text{subj. to} & \\ & M U(k) \leq W(k) + E x(k), \end{aligned}$$

Control matching

Solve the “unconstrained” problem

$$J(x(k), \omega(k), U(k)) = \min_{U(k)} U(k)^T H U(k) \\ + 2x(k)^T F U(k) + x(k)^T Y x(k)$$

The solution is $U^*(k) = -H^{-1}F^T x(k)$ and the feedback control law is

$$u^*(k) = u(0|k) = -\Lambda H^{-1}F^T x(k),$$

where $\Lambda = [\ I \ 0 \ \cdots \ 0 \]$.

“Match” the controller by finding the weighting matrices P , Q , R (hidden in H , F) such that

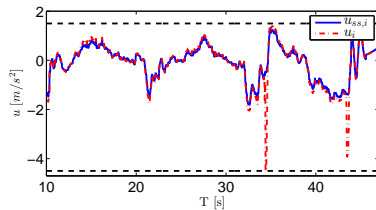
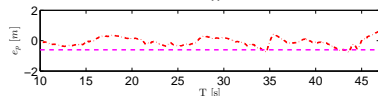
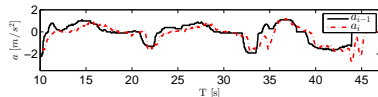
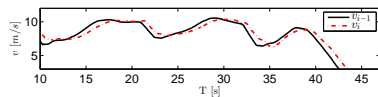
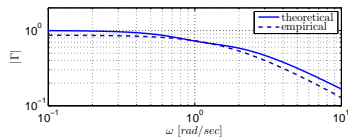
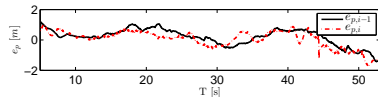
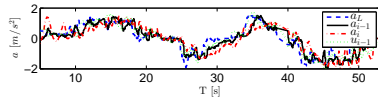
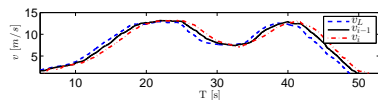
$$u_{ss}(k) = [K_{FB} K_{FF}] \tilde{x}(k) = -\Lambda H^{-1}F^T \tilde{x}(k)$$

Note that, the obtained MPC controller can guarantee string stability as long as constraints are not active.

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Experimental results



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