

A 93dB 1Ms/s Sigma-Delta ADC dissipating 8.7fJ per conversion step

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Topics of Discussion

- ❑ Analog to Digital Conversion
- ❑ Sigma-Delta Modulation
- ❑ Case Study: Design and Simulations
- ❑ Measurement Issues

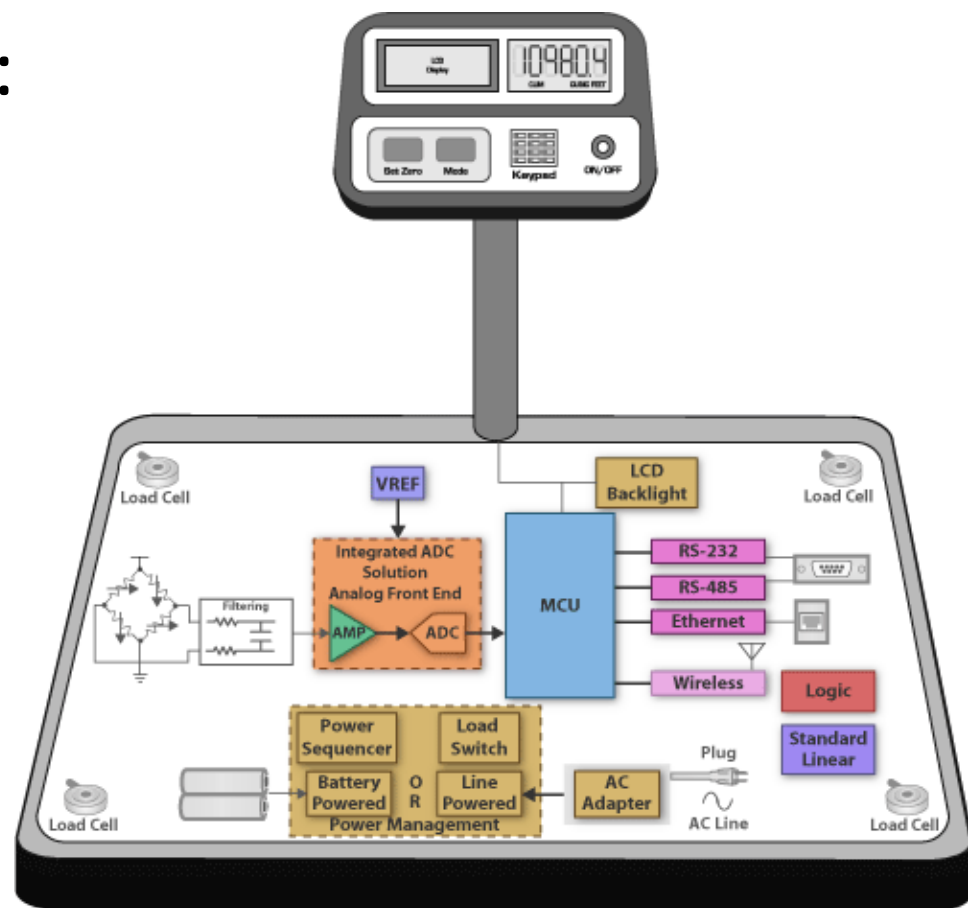
Analog to Digital Conversion

- ❑ Conversion of Signal from the Analog to the Digital Domain.
- ❑ Digital signals are transmitted in a more efficient way than analog signals.
- ❑ Applications:
 - Computers, Engineering Instrumentations (Oscilloscope...), Biomedical Instrumentations (Radar Imaging...), Music Reproduction...

A/D Conversion: Example

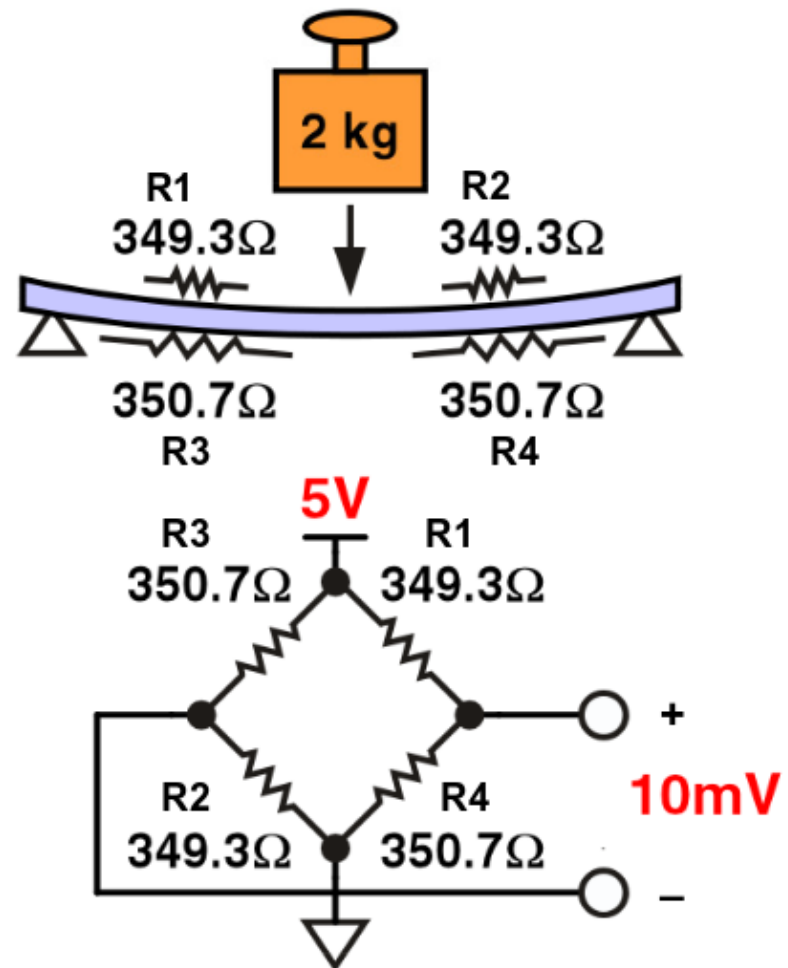
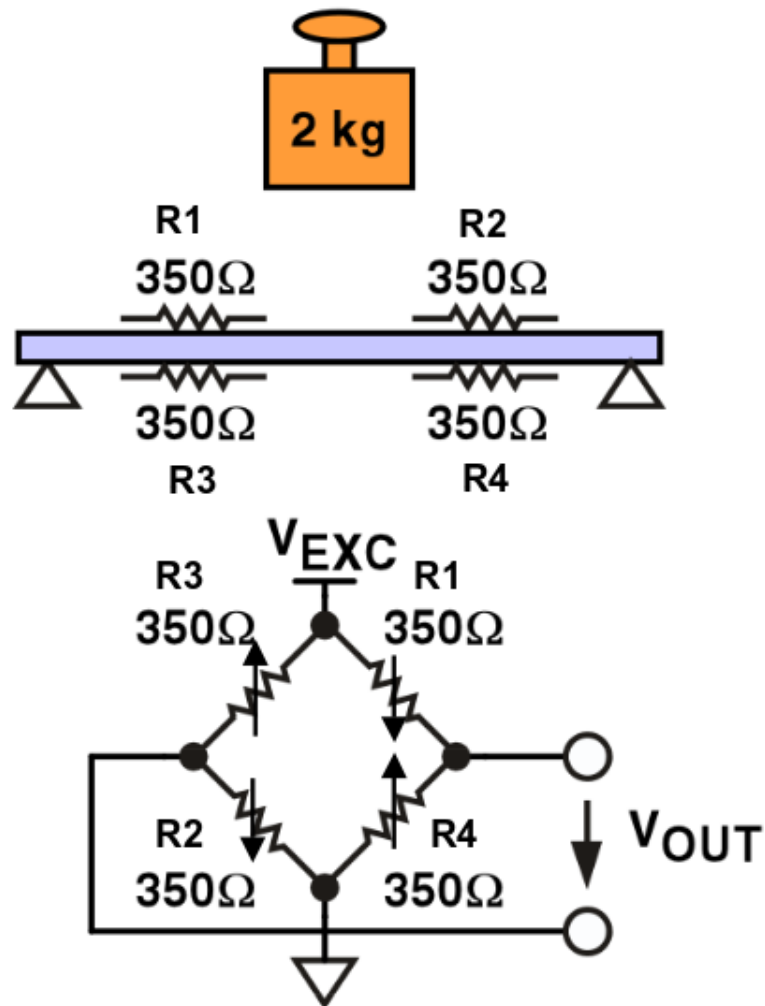
□ Weigh Scale Example:

- Capacity: 2kg
- Sensitivity: 0.1g
- Max $V_{EXC} = 10V$
- Sensitivity = 2mV/V



LEGEND	
■	Logic
■	Processor
■	Interface
■	Power
■	ADC/DAC
■	RF/IF
■	Clocks
■	Other

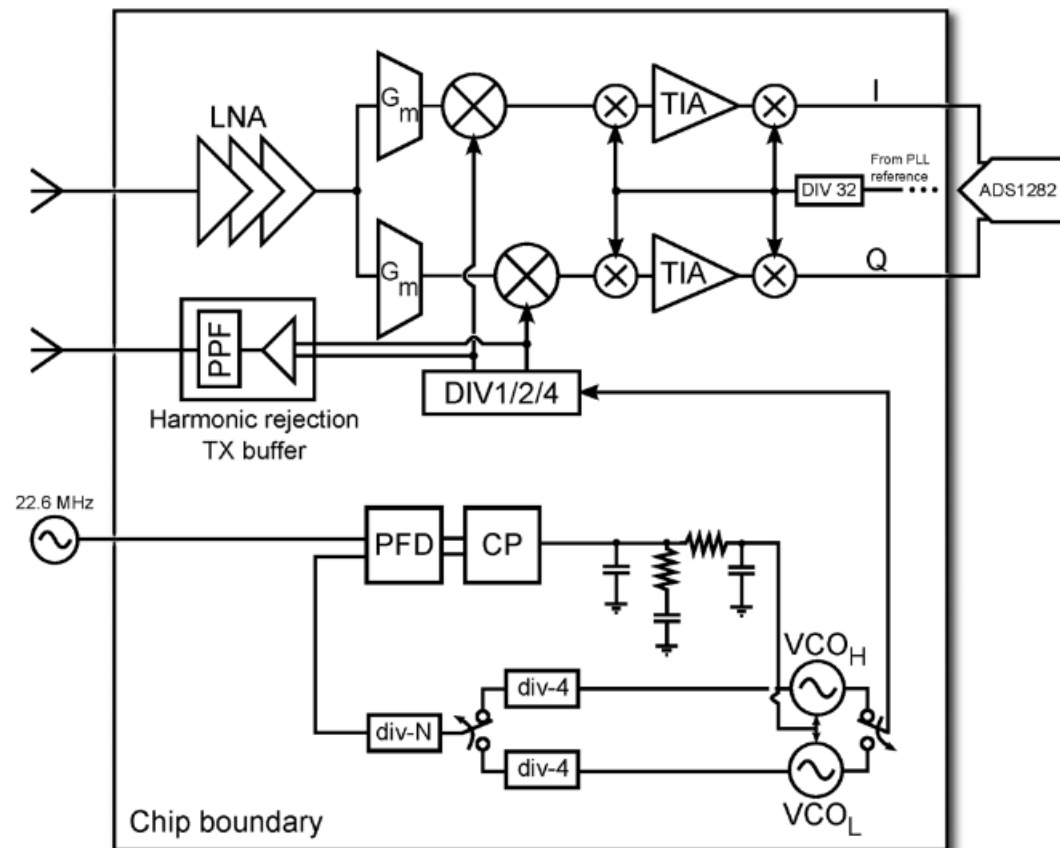
Wheat Stone Bridge



ADC Requirements

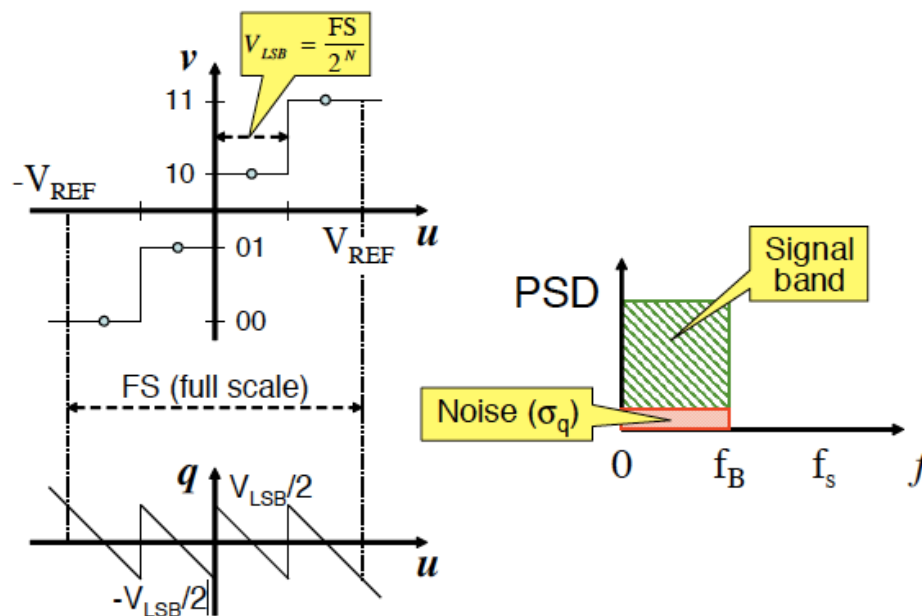
- ❑ Required 0.1g in 2kg:
 - # counts = full-scale / resolution
 - # counts = 2000 g / 0.1 g = 20.000
- ❑ 20.000 counts:
 - $V_{FS} = 10 \text{ mV @ } 5\text{V excitation}$
 - $V_{PP} = V_{FS} / \# \text{ counts} = 0.5\mu\text{V}$
- ❑ Noise-Free Code Resolution
 - $\log_{10}(V_{FS}/V_{PP}) / \log_{10}(2) = 14.3 \text{ bits}$
- ❑ RMS Noise (Gaussian Noise)
 - $V_{RMS} = V_{PP}/6.6 = 75\text{nV}$ (6.6 used to convert peak-to-peak noise to rms noise for a confidence level of 99.9%)
- ❑ Noise Code Resolution
 - $\log_{10}(V_{FS}/V_{RMS}) / \log_{10}(2) = 17 \text{ bits}$

Breast Cancer Radar Imaging



- ❑ 10-30% of tumors are missed by mammography.
- ❑ UWB microwave radar technology is an attractive alternative.
- ❑ In order to recreate an high resolution map of the breast tumors an high resolution ADC is necessary.

Analog to Digital Conversion

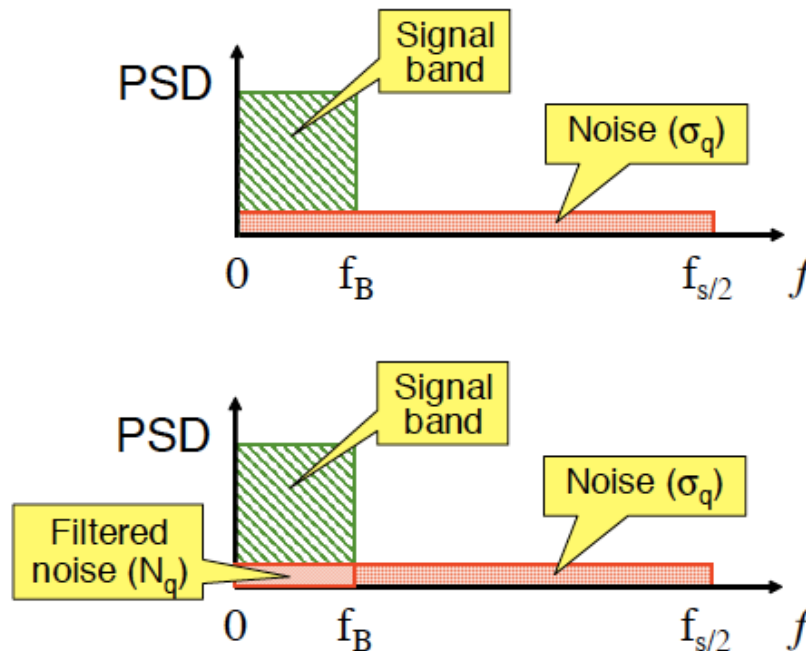


$$SNR = \frac{P_{sig}}{\sigma_q^2}$$

❑ ADC: Sampling and Quantizing. In the quantization process we introduce an error.

$$\sigma_q^2 = \frac{V_{LSB}^2}{12}; \quad P_{sig} = \left(\frac{V_{LSB} \cdot 2^N}{2\sqrt{2}} \right)^2 \rightarrow SNR = 6.02 \cdot N + 1.76\text{dB}$$

First improvement: Oversampling

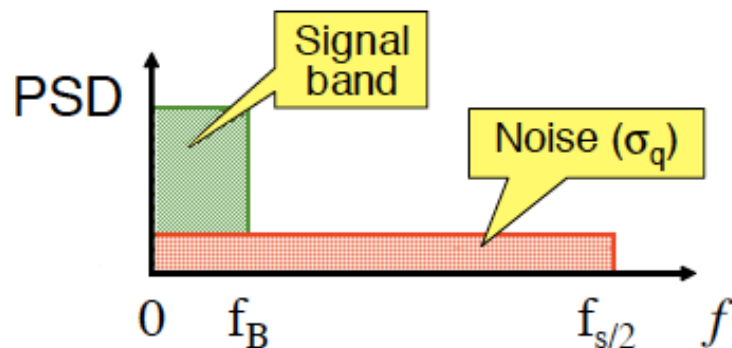


$$OSR = \frac{f_s/2}{f_B}$$

- Sampling frequency significantly higher than the Nyquist rate.

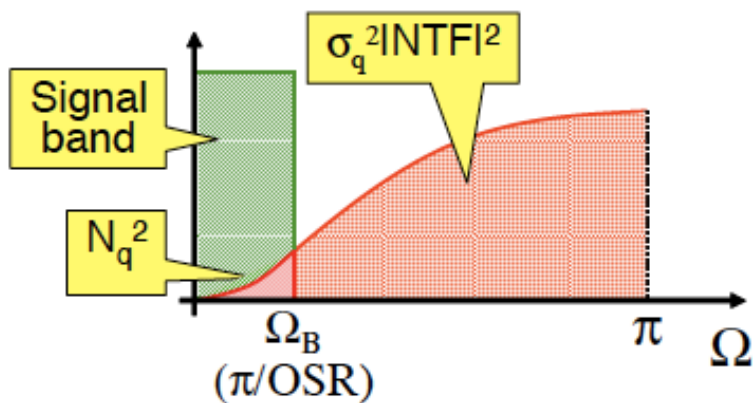
$$N_q^2 = \frac{V_{LSB}^2}{12 \cdot OSR} \rightarrow SNR = 6.02 \cdot N + 1.76\text{dB} + 10 \cdot \log OSR$$

Second Improvement: Noise Shaping (1/2)



❑ Pushing part of the quantization noise outside the signal bandwidth.

❑ High-pass filtering the quantization noise (Noise-Transfer-Function)



Second Improvement: Noise Shaping (2/2)

$$NTF(s) = \frac{s}{s+1} \leftrightarrow NTF(z) = (1 - z^{-1})$$

$$\begin{aligned} |NTF(e^{j\omega t})| &= |1 - e^{-j\omega t}| = |e^{-j\omega T/2}(e^{j\omega T/2} - e^{j\omega T/2})| \\ &= 2|\sin(\omega T/2)| = 2|\sin(\pi f T)| \end{aligned}$$

$$\begin{aligned} N_q^2 &= \int_0^{f_b} \frac{V_{LSB}^2}{12} \frac{2}{f_s} \left[2 \cdot \sin\left(\pi \frac{f}{f_s}\right) \right]^2 \cong \int_0^{f_b} \frac{V_{LSB}^2}{12} \frac{2}{f_s} \left[2 \cdot \left(\pi \frac{f}{f_s}\right) \right]^2 \\ &= \frac{V_{LSB}^2}{12} \cdot \frac{\pi^2}{3} \cdot \frac{1}{OSR^3} \end{aligned}$$

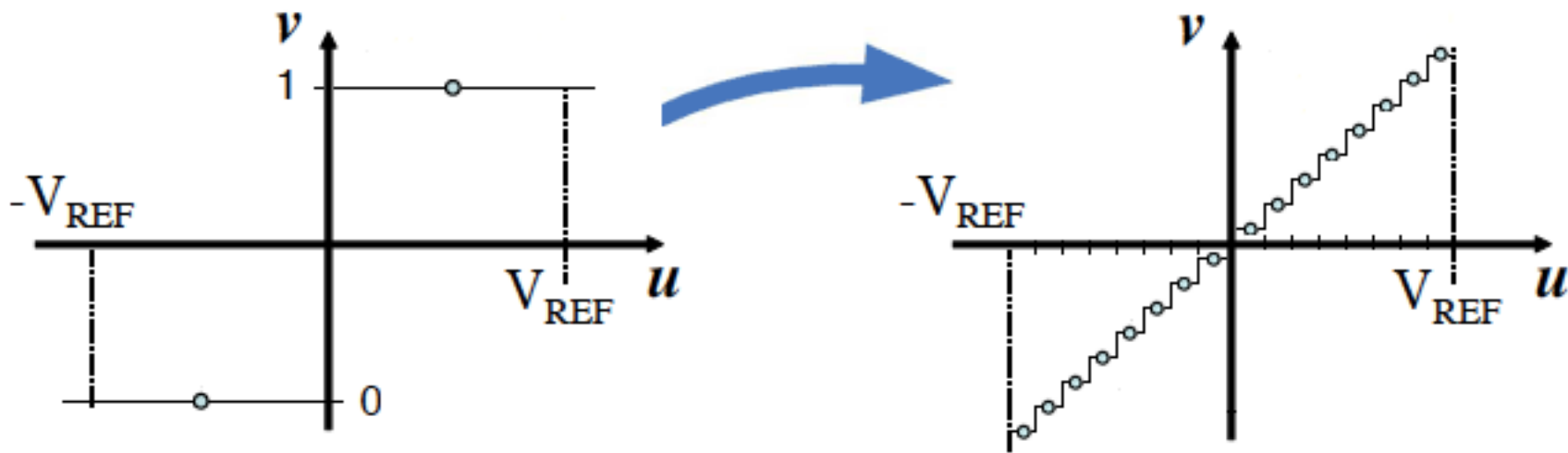
$$SNR = 6.02 \cdot N + 1.76\text{dB} - 5.2\text{dB} + 30 \log OSR$$

How 1-bit ADC achieves more than a 16-bit resolution

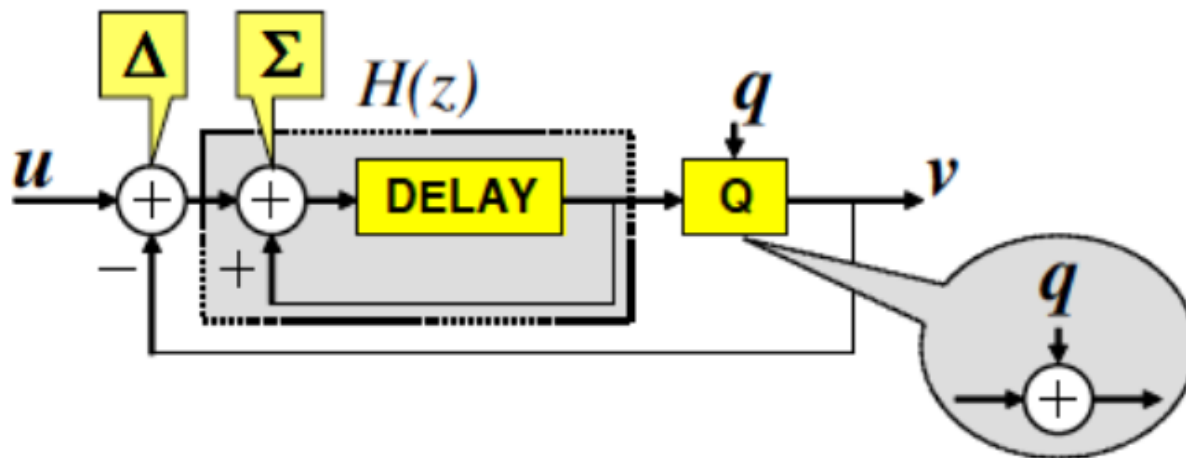
SNR in First-Order Sigma-Delta

$$SNR = 6.02 \cdot N + 1.76\text{dB} - 5.2\text{dB} + 30 \log OSR$$

□ $N = 1$, $OSR = 1024 \rightarrow SNR = 93 \text{ dB}$ (16 bit)



Sigma-Delta Modulation

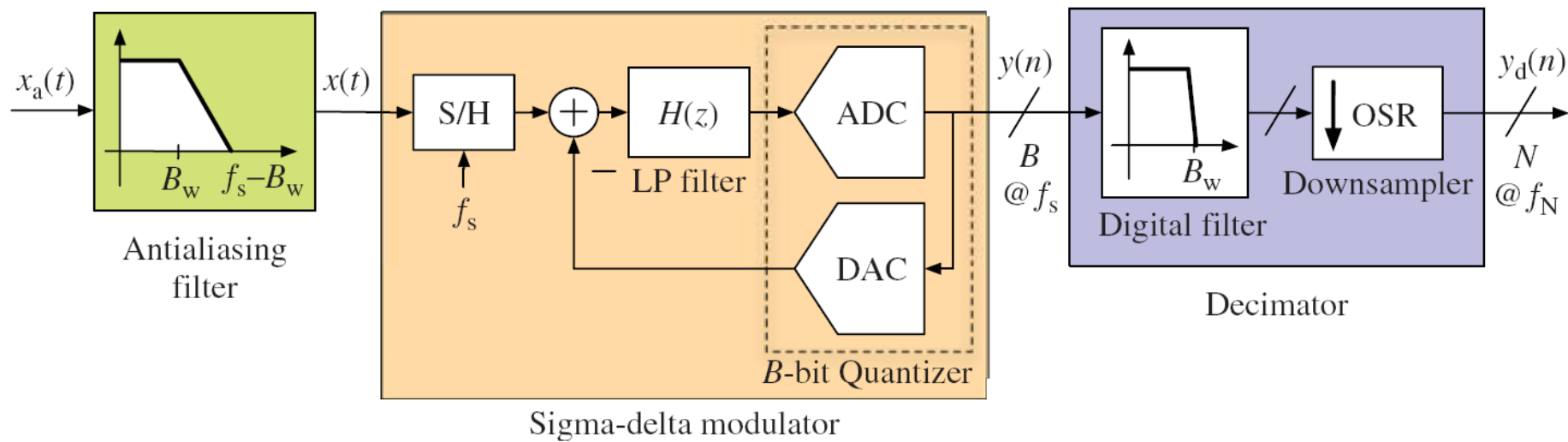


- ❑ Modeling the quantization noise as an additive quantity.

Noise Transfer Function (NTF) and Signal Transfer Function (STF)

$$\frac{v}{q} = \frac{1}{1 + H(z)} = 1 - z^{-1} \quad \text{and} \quad \frac{v}{u} = \frac{H(z)}{1 + H(z)} = z^{-1}$$

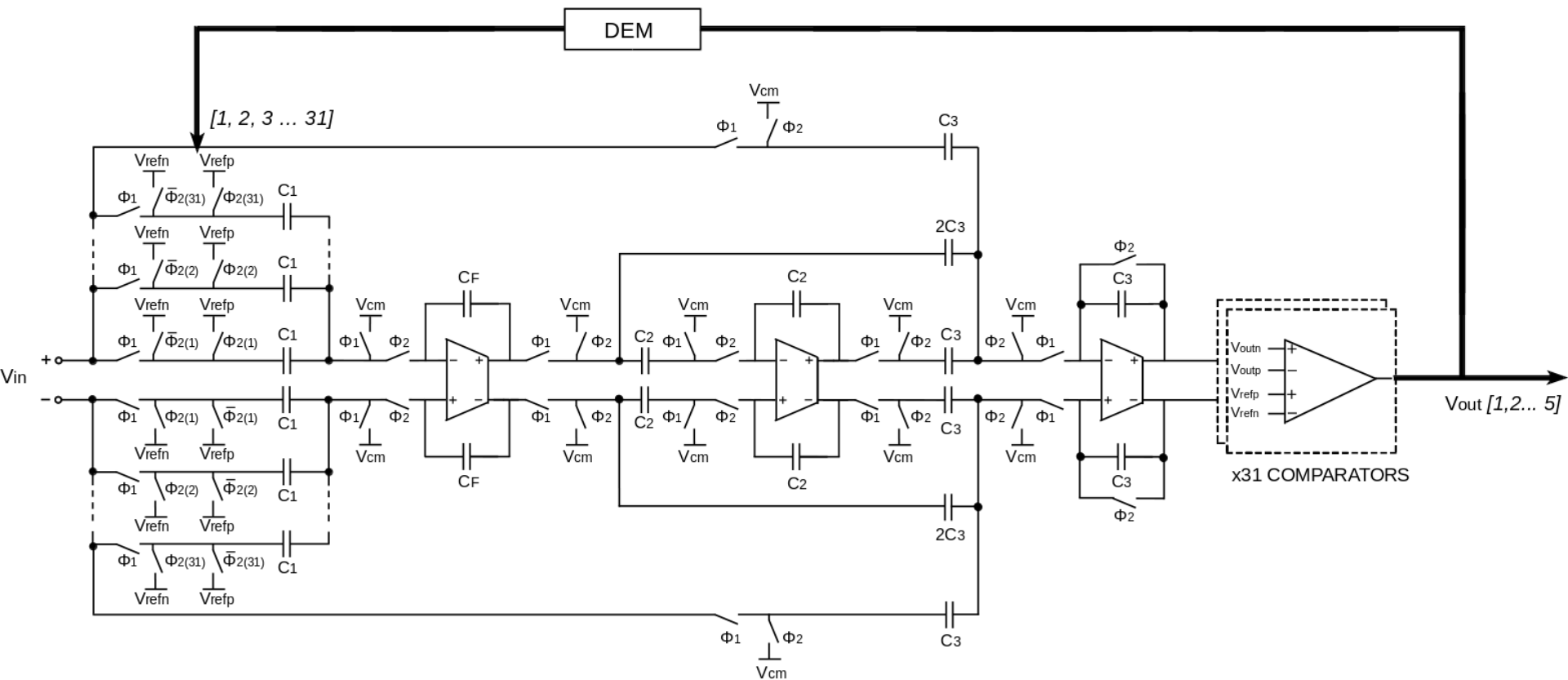
Sigma-Delta Architecture



- ❑ Digital Filter to remove the noise outside the signal bandwidth.
- ❑ DAC in the feedback path to return into analog domain.

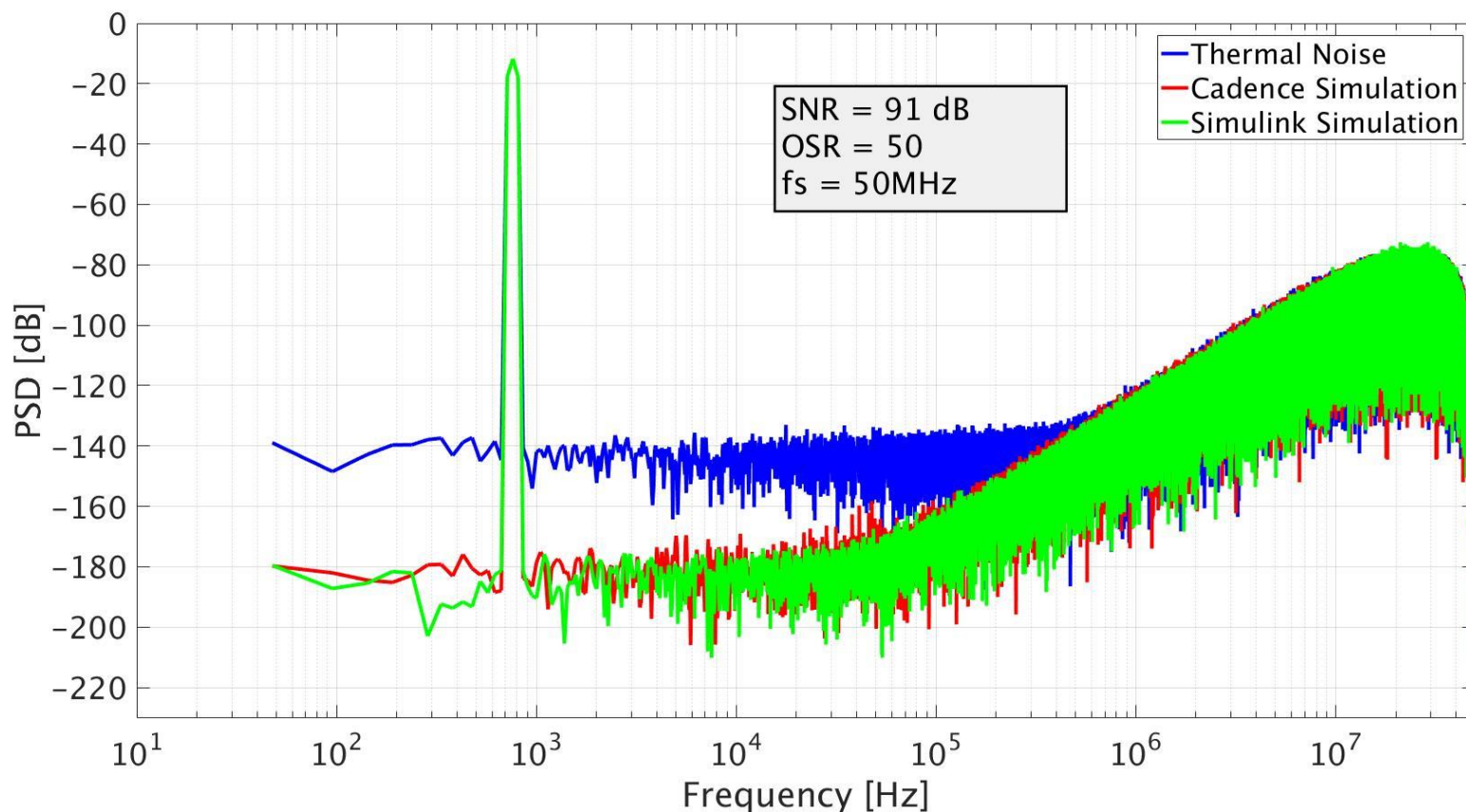


Schematic Second Order Sigma Delta

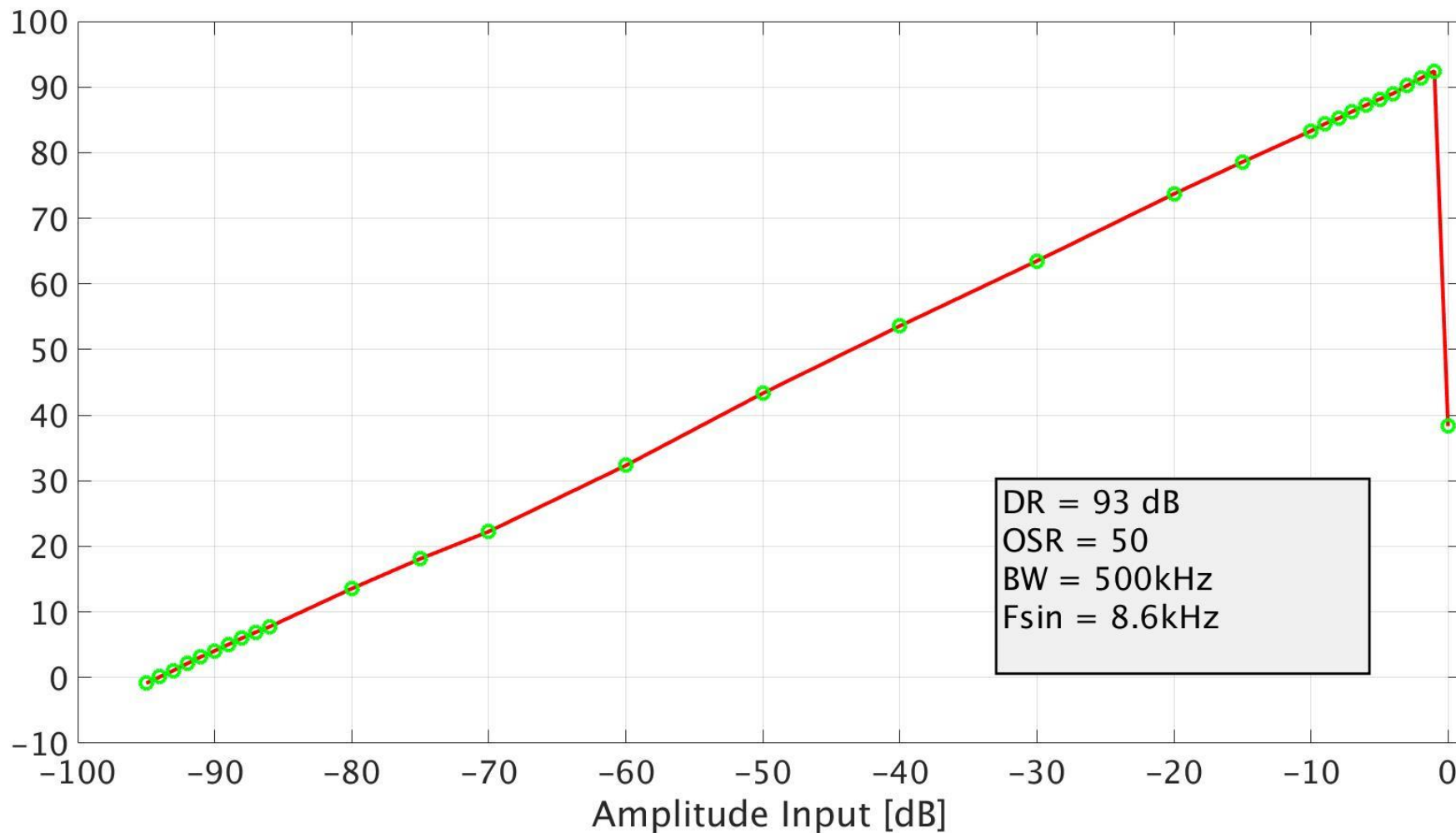


Simulations – output spectrum

- Comparison between the behavioral model and the Cadence simulation.



Simulations – dynamic range



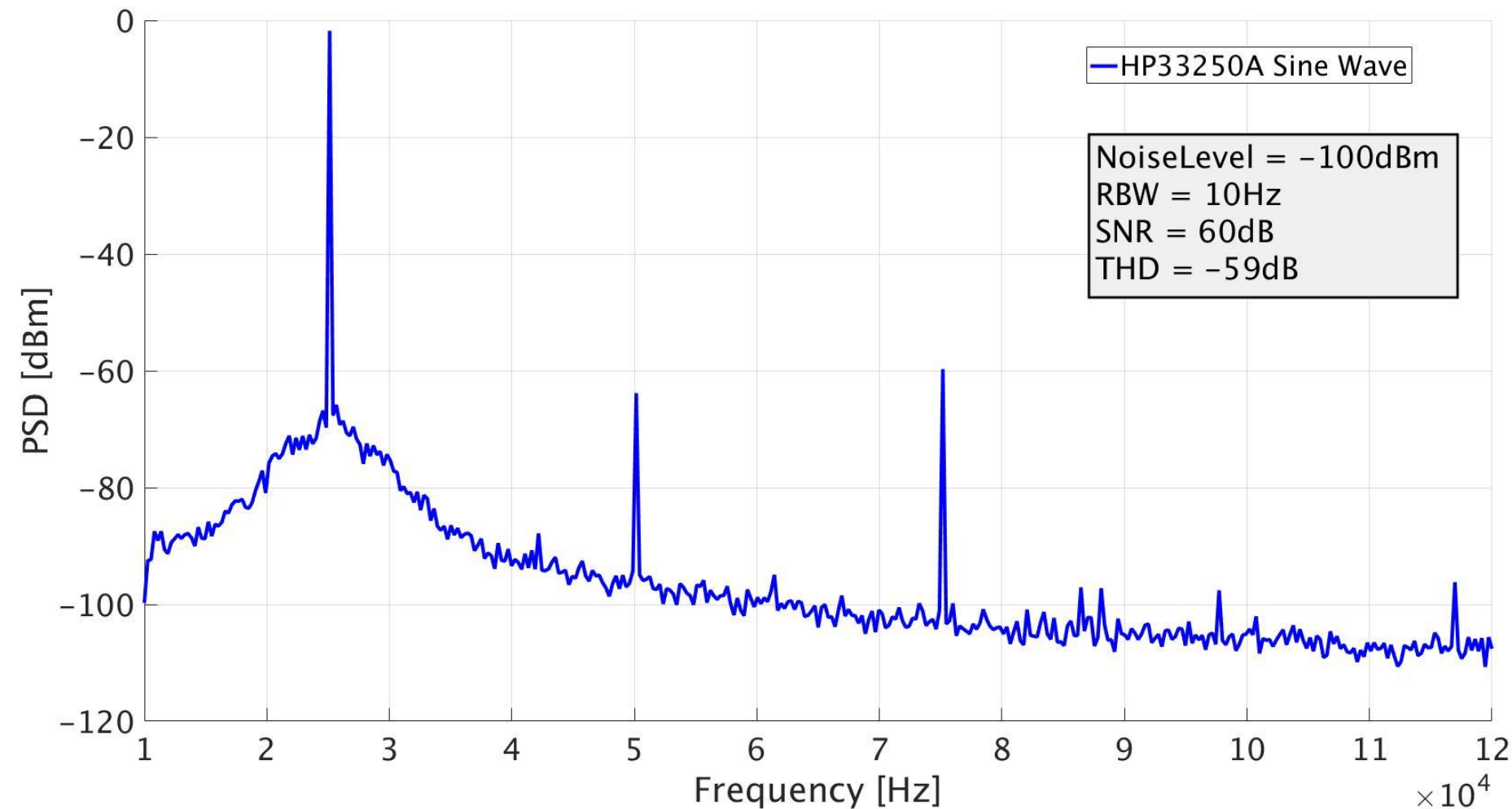
- ❑ Core area:
500μm x 480μm
- ❑ Area with PAD & decoupling caps:
1mm x 1mm

The chip has been fabricated thanks to ST Microelectronics in Lund (Sweden) and in particular thanks to prof. Pietro Andreani.

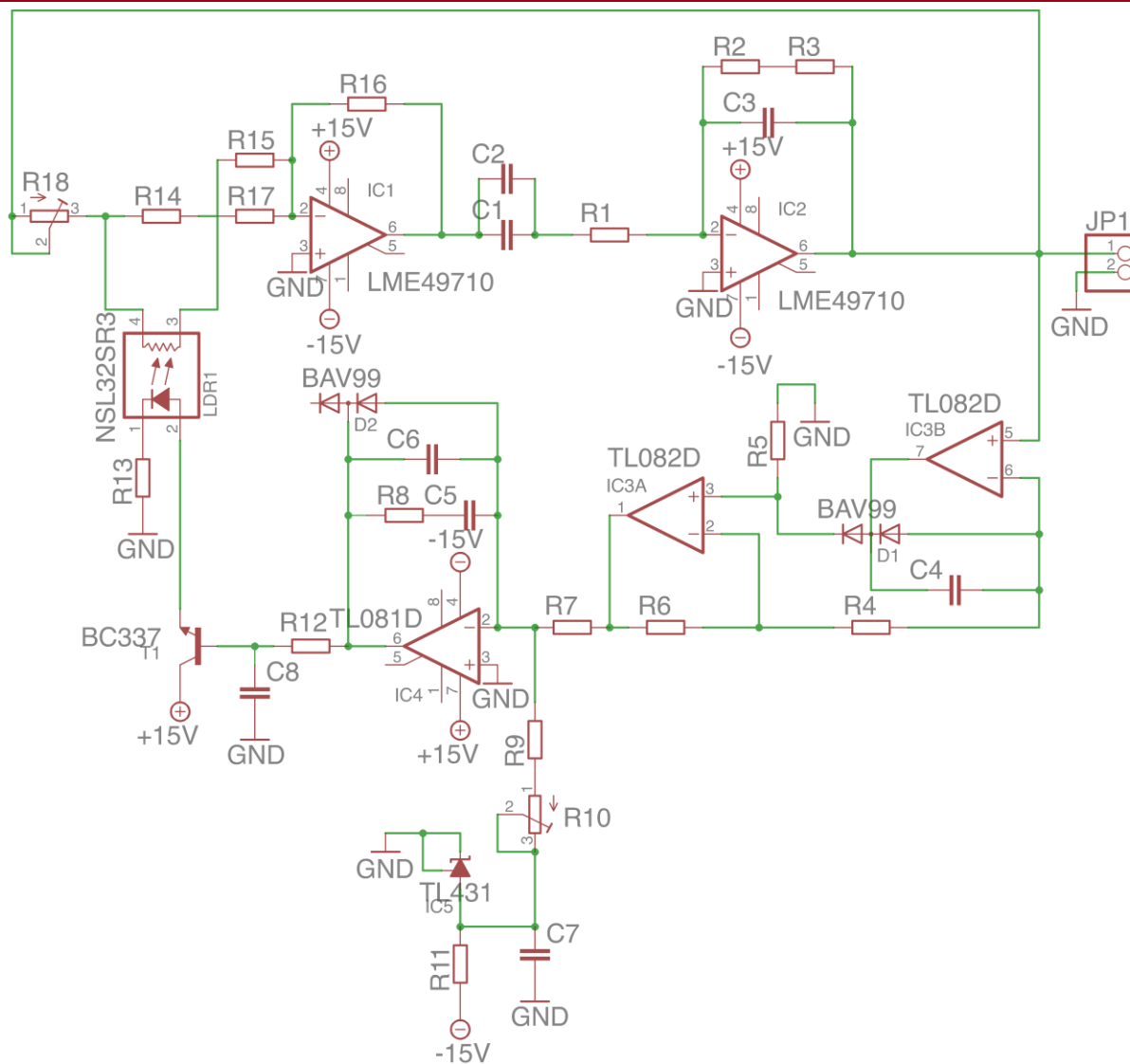
ADC Testing: Measurement Issues

- ❑ In order to test the linearity of the ADC a “pure” sinewave has to be used.
- ❑ Usually the instruments does not guarantee more than 12 bits of linearity.
- ❑ We have to create a low distortion and low noise oscillation to measure the effective resolution of the ADC.

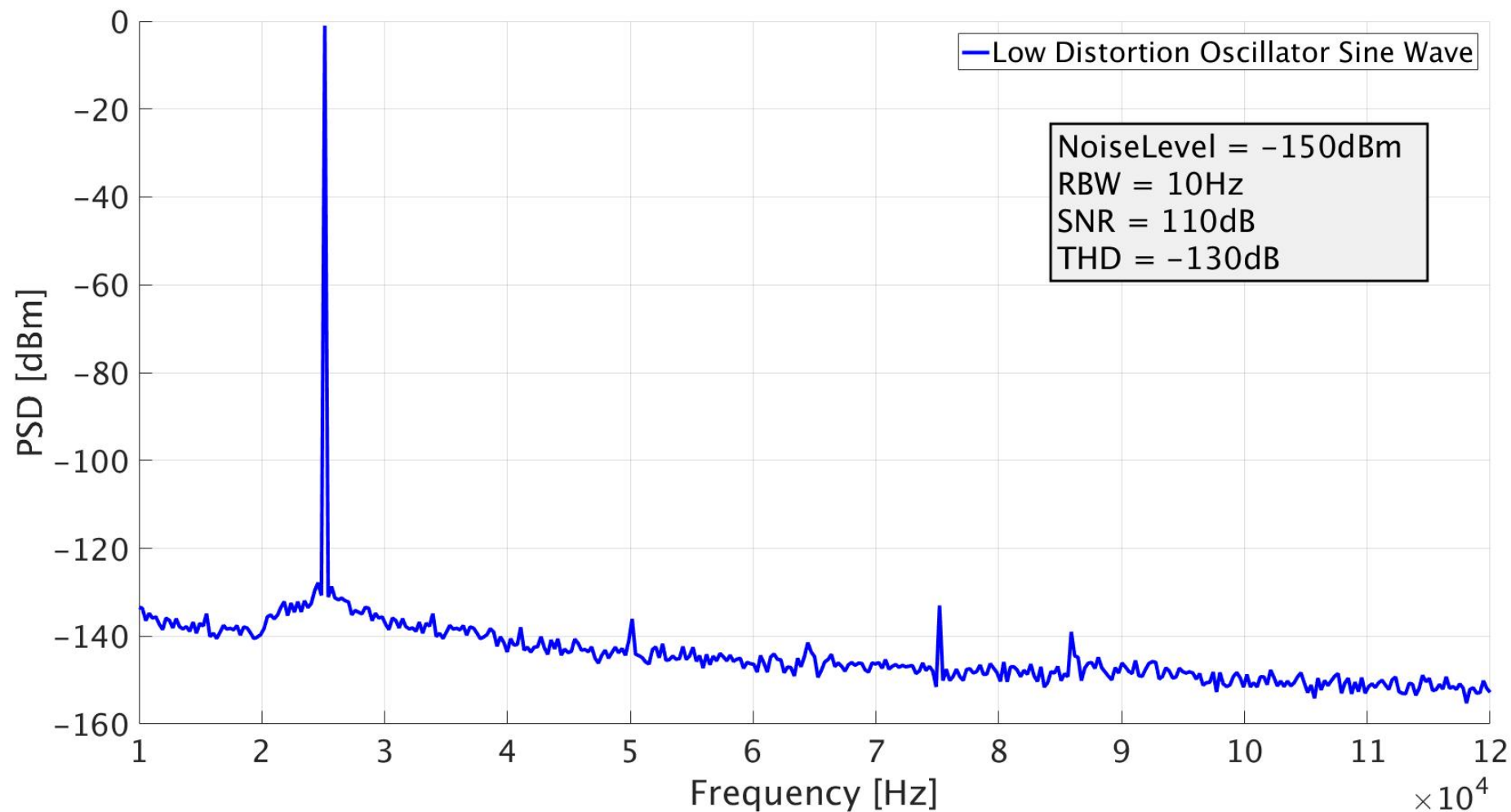
HP33250A Signal Generator Spectrum



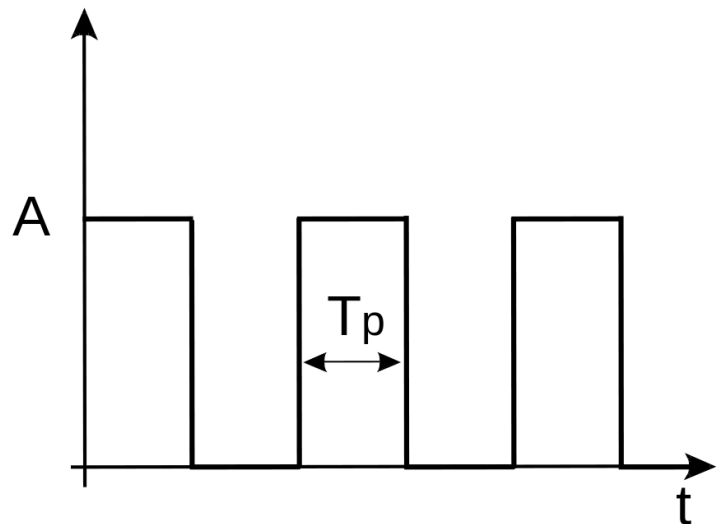
Variable Frequency Oscillator



Measured Output Spectrum



Harmonic Content of Square Wave

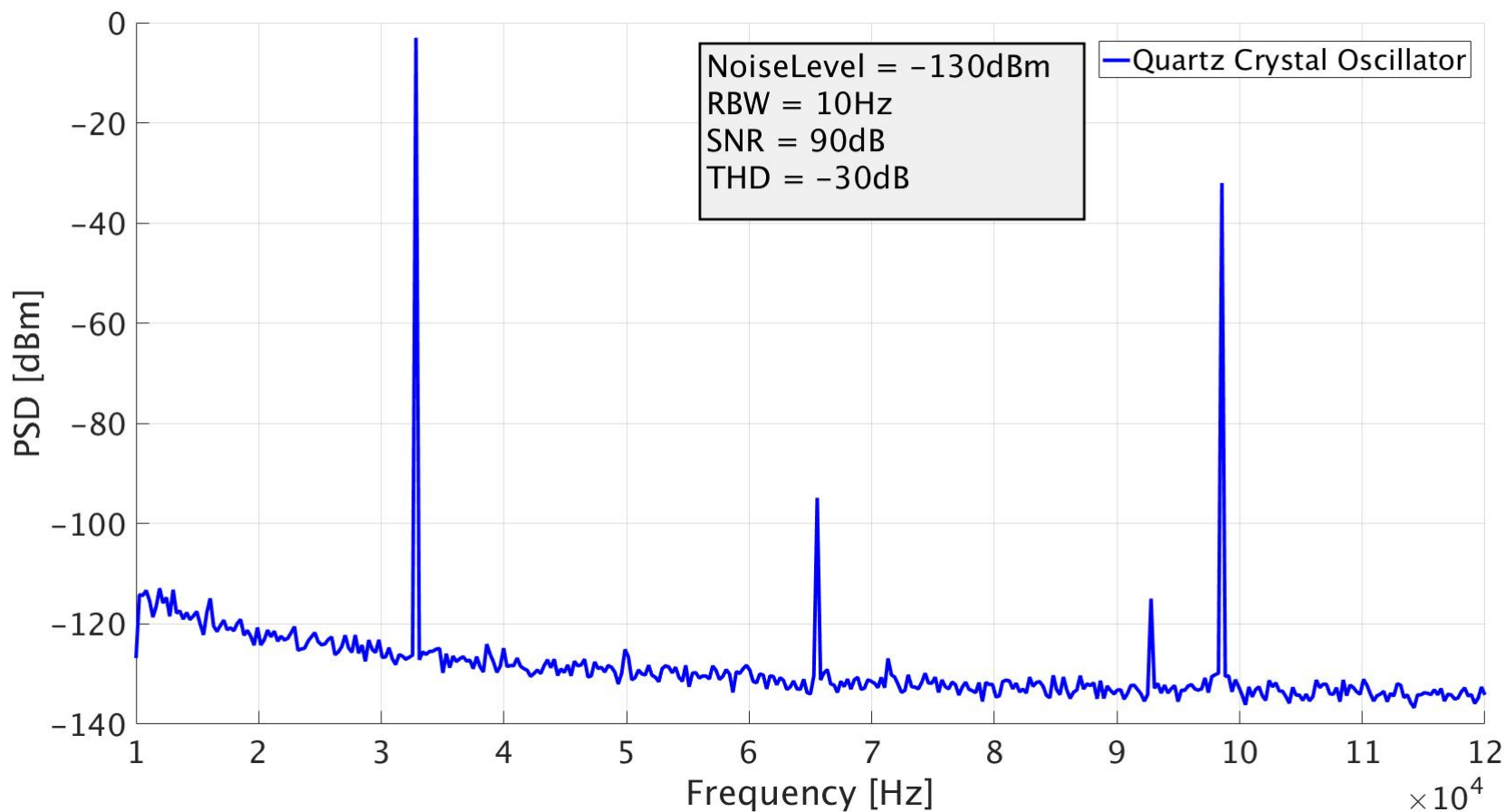


$$x(t) = \begin{cases} A & \text{if } |t| < T_p/2 \\ 0 & \text{if } |t| > T_p/2 \end{cases}$$

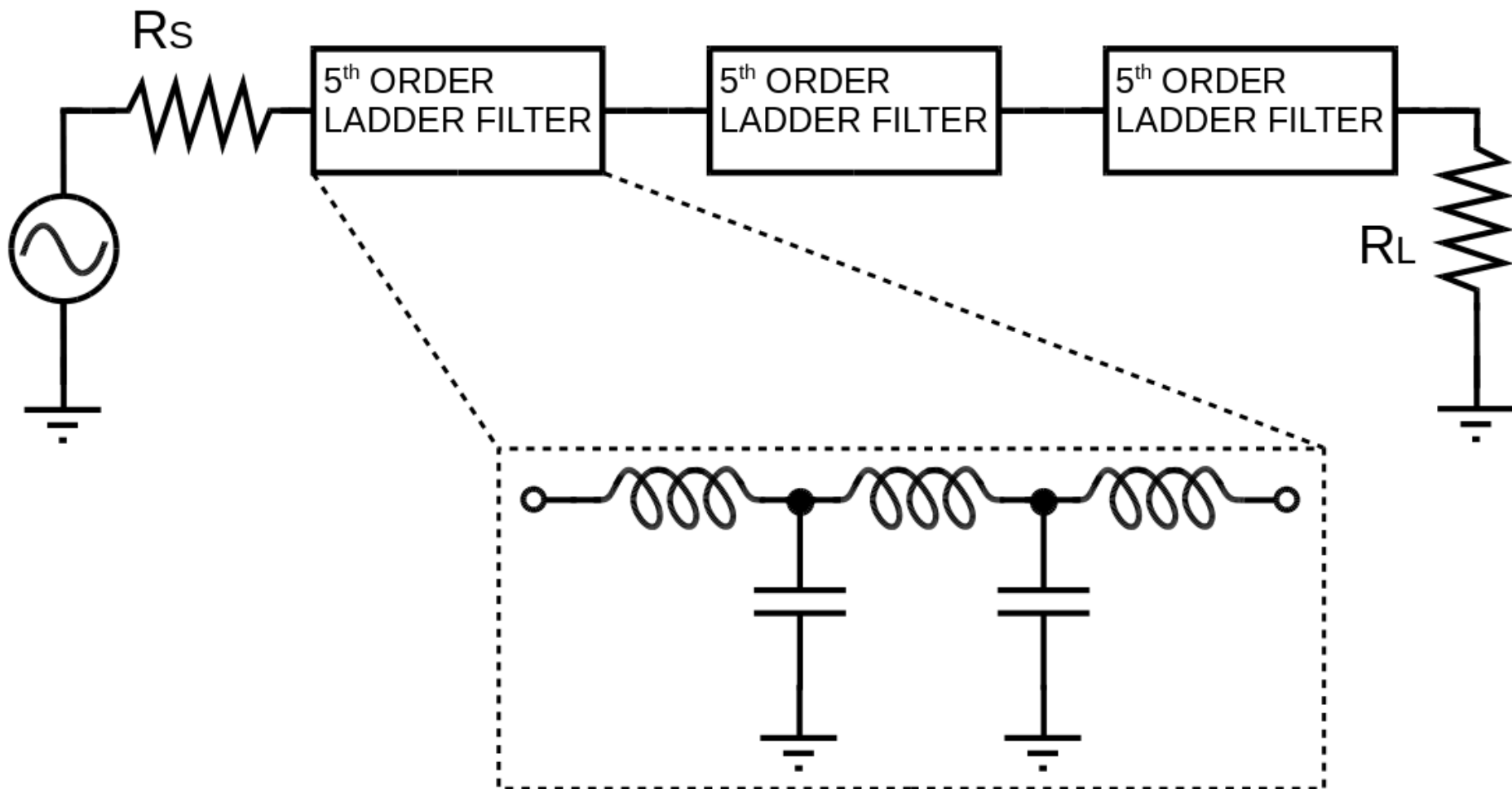
$$x(t) = \sum_{n=0}^{n=\infty} a_n \cos(n\omega_0 t)$$

$$a_n = \frac{2}{T} \int_T x(t) \cos(n\omega_0 t) dt = 2 \frac{A}{n\pi} \sin\left(\frac{n\pi}{2}\right)$$

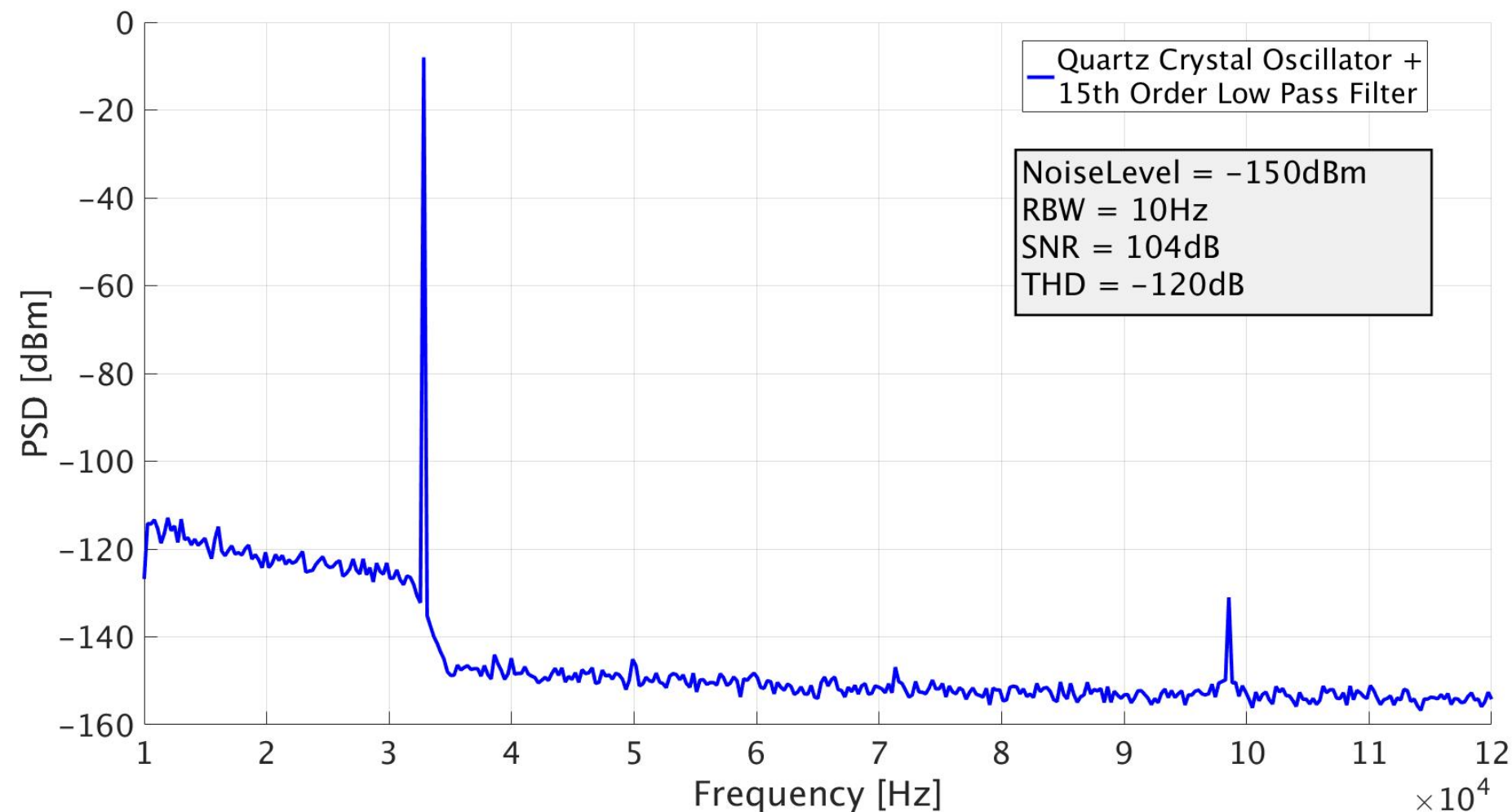
Quartz Crystal Oscillator Spectrum



Low Pass Ladder Filter



Quartz Crystal Oscillator (Filtered) Spectrum



Conclusion

- ❑ An original design of a Sigma Delta with 93 dB DR has been proposed.
- ❑ Some of the basic characteristics of the Sigma Delta topology has been highlighted.
- ❑ Low cost / high precision oscillator solutions has been proposed in order to create an ultra pure sine wave.
- ❑ Measurements are in progress in this period.